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(54) **THREE-LAYER LAMINATED FILM.**

(57) A heat-sealing three-layer laminated film having highly sealing properties, which is not easily broken even under reduced pressure, is provided. The said three-layer laminated film is characterized in that three layers including a biaxial orientation film base layer (A) made of crystalline polypropylene, a cushion layer (B) made of olefin polymer film having a melting point lower than that of the base layer (A) and a heat seal layer (C) made of olefin polymer film are laminated in the order to (A), (B) and (C), degrees of surface orientation of the respective layers are within the range of satisfying the following expressions and, when the cushion layer (B) and the heat seal layer (C) are identical in composition with each other, the degree of plane orientation of the cushion layer (B) is smaller than that of the heat seal layer (C).  $2.0 \leq P_A \leq 15.0$ ;  $0 \leq P_B \leq 3.5$ ;  $2.0 \leq P_C \leq 4.0$ ; where  $P_A$ : the degree of plane orientation of the base layer (A),  $P_B$ : the degree of plane orientation of the cushion layer (B),  $P_C$ : the degree of plane orientation of the heat seal layer (C).

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Industrial Utilization Field

The present invention relates to a laminated three-layer film and more particularly to a heat-sealable film superior in sealability under a reduced pressure.

Prior Art

In conventional laminate films superior in heat-sealability, in the case where a biaxially oriented film (A) of polypropylene is used as a base layer, a heat-sealing layer (C) is laminated to only one side of the base layer (A) to provide a (A)/(C) laminate film, or the heat-sealing layer (C) is laminated to both sides of the base layer (A) to provide a (C)/(A)/(C) laminate film, or different heat-sealing layers (C) and (C') are laminated to both sides of the base layer (A) to provide a (C)/(A)/(C') laminate film. In all of these cases, the base layer and the heat-sealing layer(s) are in contact with each other. (See Japanese Patent Laid Open No. JP53-128685A and Patent Publication No. JP59-26470B.)

Object of the Invention

Such conventional laminate films superior in heat-sealability have been disadvantageous in that when the atmospheric pressure changes from a normal pressure to a reduced pressure, for example when the films are exposed to the air of a high ground during transport over a mountain, there occurs cleavage at the interface between the base layer (A) and the heat-sealing layer (C) or (C'), which is apt to cause bursting of the bags formed by the films.

It is the object of the present invention to solve such a problem of the prior art and provide a laminated three-layer film superior in heat-sealability and difficult to burst even under a reduced pressure.

Summary of the Invention

The laminated three-layer film according to the present invention is characterized in that a base layer (A) which is a biaxially oriented film formed of a crystalline polypropylene, a cushion layer (B) which is a film of an olefin polymer lower in melting point than the base layer (A), and a heat-sealing layer (C) which is an olefin polymer film, are laminated together in the order of (A)/(B)/(C), that the three layers are in the following ranges in terms of the degree of surface orientation, and that when the cushion layer (B) and the heat-sealing layer (C) are of the same composition, the degree of surface orientation of the cushion layer (B) is smaller than that of the heat-sealing layer (C):

$$2.0 \leq P_A \leq 15.0$$

$$0 \leq P_B \leq 3.5$$

$$2.0 \leq P_C \leq 4.0$$

where,

$P_A$ : degree of surface orientation of the base layer (A)

$P_B$ : degree of surface orientation of the cushion layer (B)

$P_C$ : degree of surface orientation of the heat-sealing layer (C)

Preferred Embodiments of the Invention

In the base layer (A) of a biaxially oriented film formed of a crystalline polypropylene in the present invention, the polypropylene is preferably a homopolymer (hereinafter referred to simply as "PP"), but it may be a copolymer of propylene and a small amount of another  $\alpha$ -olefin. In view of the rigidity and stretchability required for the base layer, it is preferable for the polypropylene to have a melting point not lower than 155°C and an intrinsic viscosity  $[\eta]$  of 1.5 to 2.5 dl/g. The biaxial orientation of the base layer is obtained by a conventional biaxial orienting method. It is optional which of simultaneous biaxial stretching and sequential biaxial stretching is to be adopted, provided it is necessary that the degree of surface orientation  $P_A$  should be in the range of 2.0 to 15.0, preferably 2.5 to 13.0.

The surface orientation degrees ( $P_A$ ,  $P_B$ ,  $P_C$ ) are determined at absorbance ratios  $d_{841}/d_{890}$  and  $d_{841}/d_{810}$  according to Laser Raman microscopy. An in-plane difference in the degree of surface orientation,  $\Delta P_A([P_{TD}-P_{MD}])$ , which is also determined by the same Laser Raman microscopy, is not specially limited if only the degree of surface orientation is within the foregoing range. It is well known that the closer to zero,

the better the length-breadth balance of film. But in the case of a film obtained by sequential biaxial stretching, a suitable  $\Delta P_A$  value is in the range of 0 to 13, preferably 6 to 12. If  $P_A$  is smaller than 2.0, preferably smaller than 2.5, the resulting laminate film will be low in rigidity and difficult to effect packaging, and if it exceeds 15.0, preferably 13.0, the adhesive force of printing ink will be deteriorated.

5 The cushion layer (B) formed in contact with the base layer (A) in the invention is characterized by being low in the degree of surface orientation  $P_B$ , which is in the range of 0 to 3.5, preferably not larger than 3.0, more preferably not larger than 2.5. If  $P_B$  of the cushion layer (B) exceeds 3.5, the cushioning property between the base layer (A) and the heat-sealing layer (C) will be deteriorated, thus leading to deterioration in the sealability under a reduced pressure. The polymer which constitutes the cushion layer (B) is an olefin  
10 polymer having a degree of surface orientation which falls under the foregoing range and having a melting point lower than that of the base layer (A). Preferably, the melting point of the polymer is in the range of 80° to 155°C. Examples are homopolymers of  $\alpha$ -olefins (e.g. polyethylene), copolymers of  $\alpha$ -olefins (e.g. ethylene-propylene copolymer, ethylene-butene copolymer, ethylene-propylene-butene copolymer), as well as such olefin copolymers as ethylene-vinyl acetate copolymer and ethylene-acryl monomer copolymer.  
15 Ethylene copolymers are preferred. Particularly, ethylene-propylene-butene copolymer is preferred.

The cushion layer (B) may be of the same composition as the heat-sealing layer (C). But in this case, it is necessary that the degree of surface orientation of the cushion layer (B) be smaller than that of the heat-sealing layer (C). The difference in the surface orientation degree between the two is preferably not less than 0.5, more preferably not less than 1.0. That the composition is the same means that the polymer  
20 constituting monomers are the same.

The cushion layer is a layer which is sandwiched in between the base layer and the heat-sealing layer. When the bag formed by the constituent layers is about to be burst upon sudden expansion under a reduced pressure, the cushion layer absorbs the stress imposed on the base layer (A) and that on the heat-sealing layer (C) to prevent, or make it difficult, the bag from being pulled by the hard base layer and heat-seal layer and burst eventually. Thus, the cushion layer serves as a buffer. That is, it is a layer for affording  
25 a cushioning action. It is necessary for the cushion layer to be sandwiched in between the base layer (A) and the heat-sealing layer (C). If it is positioned outside (A)/(C), its cushioning action will be insufficient in practical use.

It is necessary that the heat-sealing layer (C) used in the invention should have a degree of surface  
30 orientation  $P_C$  of 2.0 to 4.0, preferably 2.5 to 3.5. If  $P_C$  is smaller than 2.0, hot tack is apt to occur at the time of sealing, thus resulting in difficulty of processing, and if it exceeds 4.0, a deteriorated heat-sealing force will result. The polymer which constitutes the heat-sealing layer (C) is an olefin homopolymer or an olefin copolymer, with the latter being preferred. Examples are ethylene copolymers such as ethylene-propylene copolymer, ethylene-propylene-butene copolymer, ethylene-butene copolymer, copolymers of  
35 ethylene and acryl monomers such as acrylic acid, methyl acrylate, ethyl acrylate, methacrylic acid, methyl methacrylate and ethyl methacrylate, ethylene-maleic anhydride copolymer, terpolymers of these comonomers with maleic anhydride, and ethylene-vinyl acetate copolymer, as well as mixtures thereof. Such olefin homopolymers as polyethylene and polypropylene are also employable preferably in the form of an extruded laminate or in a laminated form of unstretched films thereof. Further, petroleum resins, wax,  
40 etc. may be incorporated in the heat-sealing layer.

In the laminated three-layer film of the present invention it is necessary that the base layer (A), cushion layer (B) and heat-sealing layer (C) be laminated in the order of (A)/(B)/(C). This construction is essential for obtaining a film superior in sealability and also in the bag-burst preventing property under a reduced pressure. Particularly, the layer (B) is a cushion layer whose surface orientation is kept to a minimum, so it  
45 is required to be sandwiched in between the base layer (A) and the heat-sealing layer (C).

It is preferable that a fatty acid amide, inorganic particles, fine silicone particles or the like, be incorporated in the range of 0.01 to 5 wt% into both surface layers, namely the base layer (A) and the heat-sealing layer (C), of the laminated three-layer film, to impart slipperiness and blocking resistance thereto.

In the three-layer film of the invention, the thickness of each layer is not specially limited. But as to the  
50 base layer (A), it is preferred that the lower limit of its thickness be 10  $\mu\text{m}$  in view of stiffness and resistance to load and the upper limit thereof be 80  $\mu\text{m}$  in view of an economic amount of polymer used per unit area. Also as to the thickness of the cushion layer (B), there is no limitation placed thereon. But when its cushioning effect is taken into consideration, it is preferred that the lower limit of its thickness be 1  $\mu\text{m}$  from the standpoint of preventing the burst of bag under a reduced pressure and the upper limit thereof  
55 be 5  $\mu\text{m}$  from the standpoint of rigidity. Further, no special limitation is imposed on the thickness of the heat-sealing layer (C), either, but it is preferred that the lower limit thereof be 2  $\mu\text{m}$  from the standpoint of sealability and prevention of bag-burst at a reduced pressure and the upper limit thereof be 25  $\mu\text{m}$  from the standpoint of rigidity.

On the base layer (A) side in the present invention, when O/C ratio is in the range of 0.1 to 0.35 and N/C ratio in the range of 0.005 to 0.05, as atomic ratios within 10 nm from the surface, there is attained an excellent printability, namely a strong adhesive force of printing ink, of the said surface, so such ranges are preferred.

5 The laminating method for the three-layer film is not specially limited. But the method of laminating the layers (A) and (B) by co-extrusion and then forming the heat-sealing layer (C) on the cushion layer (B) by extrusion or coating, can easily afford the specified ranges of surface orientation degrees and is advantageous from the economic point of view. Of course, there may be adopted a method in which the three layers are formed at a time by co-extrusion.

10 Examples of methods for preparing the laminated three-layer film of the invention will be described below, but it is to be understood that the present invention is not limited thereto.

According to a first manufacturing example, a polypropylene for constituting a base layer (A) is fed to an extruder, while a polymer for constituting a cushion layer (B) is fed to another extruder, then both are conducted to a single die, from which they are co-extruded simultaneously in a melted state at 200-300 °C and wound onto a cooling drum to obtain a two-layer sheet. Subsequently, the two-layer sheet is conducted to an oven with rolls or a roll disposed therein, in which it is stretched 3 to 7 times in the longitudinal direction under heating to 100-150 °C. Then, the sheet is conducted into a tenter, in which it is heated to 150-190 °C and stretched 5 to 15 times in the transverse (width) direction, then heat-treated and, if necessary, heat-relaxed. Thereafter, a polymer for constituting a heat-sealing layer (C) is melt-extruded and laminated at 200-300 °C onto the surface of the cushion layer (B) of the biaxially stretched two-layer film thus obtained. In this way there is obtained a laminated three-layer film falling under the scope of the present invention. Of importance is that the specific surface orientation degrees of the constituent layers as a characteristic feature of the invention are attained by combinations of the aforementioned extrusion temperatures, heating temperatures in stretching and stretch ratios of the layers. More specifically, the lower the extrusion temperature and the heating temperature in stretching, the higher the degree of surface orientation, and vice versa. Even when the extrusion temperature and the heating temperature in stretching are the same, the degree of surface orientation is low if the stretch ratio is low and it is high if the stretch ratio is high. Thus, the ranges of the surface orientation degrees defined in the present invention are obtained by combinations of such extrusion temperatures, heating temperatures in stretching and stretch ratios. The said ranges depend on polymers used for forming the base layer (A), cushion layer (B) and heat-sealing layer (C), as well as the melting points of the polymers. Then, if necessary, a known corona discharge treatment in the air or in nitrogen and/or carbon dioxide may be applied to the surface of the base layer (A) in the three-layer film thus obtained. This treatment is preferred for imparting an ink adhesive force to the base layer surface.

35 According to another example of a manufacturing method employable in the invention, a polypropylene for constituting a base layer (A) is fed to an extruder, while a polymer for constituting a cushion layer (B) is fed to another extruder, then both are conducted to a single die, from which they are co-extruded simultaneously in a melted state at 200-300 °C and wound onto a cooling drum to obtain a two-layer sheet. Subsequently, the two-layer sheet is conducted into an oven with rolls or a roll disposed therein, in which the sheet is heated to 100-150 °C and stretched 3 to 7 times in the longitudinal direction. Further, a polymer for constituting a heat-sealing layer (C) is melt-extruded and laminated at 200-300 °C from a still another extruder onto the surface of the cushion layer (B) in the thus longitudinally uniaxially oriented sheet to obtain a three-layer sheet. Then, the three-layer sheet is conducted into a tenter, in which it is heated to 150-190 °C and stretched 5 to 15 times in the transverse (width) direction, then heat-treated and, if necessary, heat-relaxed to afford a laminated three-layer film according to the present invention. In this case, what is important is that the specific ranges of the surface orientation degrees of the constituent layers as a characteristic feature of the present invention are attained by combinations of the above melt-extrusion temperatures, heating temperatures in stretching and stretch ratios of the layers as in the foregoing first manufacturing example. Inevitably, such ranges depend on polymers used for forming the base layer (A), cushion layer (B) and heat-sealing layer (C) and their melting points. But the correlation between each temperature, stretch ratio and the degree of surface orientation obtained shows the same tendency as in the first manufacturing example. Then, where required, the surface of the base layer (A) in the three-layer film is subjected to the foregoing corona discharge treatment.

55 The following methods were adopted for determining characteristic values and effects in the present invention.

## (1) Degree of Surface Orientation

Using Laser Raman microscopy, a polarization-excited light is directed to each film layer and is received by a photomultiplier through an analyzer. Optical densities are measured at  $810\text{ cm}^{-1}$ ,  $841\text{ cm}^{-1}$  and  $890\text{ cm}^{-1}$ , then the film is rotated  $360^\circ$  and a maximum value of optical density ratios, namely absorbance ratios  $d_{841}/d_{890}$  and  $d_{841}/d_{810}$ , is determined as a degree of surface orientation. The said  $d_{810}$ ,  $d_{841}$  and  $d_{890}$  represent absorbances at  $810\text{ cm}^{-1}$ ,  $814\text{ cm}^{-1}$  and  $890\text{ cm}^{-1}$ , respectively.

## (2) Heat-Seal Strength

Using a hot plate heat-sealer and sealing bars 30 cm long by 10 mm wide, heat sealing is performed under the conditions of  $135^\circ\text{C}$ ,  $1\text{ kg/cm}^2$  pressure, 0.5 second, and a peel strength of the sealed portion is determined by means of Tensilon.

## (3) Bag-Burst Preventing Property under Reduced Pressure

This test is a kind of a cushioning property determining method. Heat-sealing faces of film are lapped together and heat sealing is performed under the conditions of  $135^\circ\text{C}$ ,  $1.0\text{ kg/cm}^2$  pressure, 0.5 second. Internal dimension of the resulting bag is set at 7 cm x 10 cm and 100 ml of air is sealed into the bag. Then, the bag is placed in a reduced pressure tester whose temperature has been controlled to  $25^\circ\text{C}$ , and is held under a vacuum of  $-350\text{ mmHg}$  for 5 minutes. The following evaluation is made in accordance with the number of burst bag out of ten such bags:

Number of Burst Bag	Evaluation
0	⊙
1~3	○
4~7	△
8 or more	X

## (4) Sealability (Bubble Test)

This test is a kind of a cushioning property determining method. Bags which have been prepared in the same manner as in the above bag-burst preventing property test under reduced pressure are placed in a constant-temperature water bath maintained at  $25^\circ\text{C}$  and are each held in a position of 15 cm from the water surface for 3 minutes. Each bag with no bubble is evaluated to be ⊙, each bag with bubble generated in 1 minute to shorter than 3 minutes is evaluated to be ○, and each bag with bubble generated within 1 minute is evaluated to be X.

The case where the above (3) and (4) are both good can be judged to be superior in cushioning property.

## (5) Rigidity (F-5 Value)

A stress-strain curve is obtained according to a Tensilon method to find a stress at 5% strain. The case where this value is  $3\text{ kg/mm}^2$  or more is judged to be superior in both rigidity and handleability with little deformation caused by tension or external stress during processing.

## (6) Hot Tack

Using a heat seal tester (a product of Toyo Tester Kogyo), the upper portion of film 15 mm wide by 300 mm long, then a load of 50 g is applied to the lower portion of the film, allowing the film to hang down in front of sealing bars. A portion of the film is folded in two, then inserted between the sealing bars and bonded (seal width: 25 mm) at a sealing temperature of  $125^\circ\text{C}$  and a sealing pressure of  $1\text{ kg/cm}^2$  for 1 second. Just thereafter, the load drops freely. A peel length (mm) of the sealed portion at a certain peeling load is measured. A value of the peel length not larger than 5 mm is judged to be good, while a value of the peel length not smaller than 20 mm is judged to be bad.

## (7) Atomic Ratio

Using ESCA 750 (a product of Shimazu Seisakusho, Ltd.) and  $MgK_{\alpha 1,2}$  as excitation X-ray, an ESCA of 1s orbit for a treated surface of film is measured while a photoelectron escape angle is set at 90 degrees and a bond energy value of  $C_{1s}$  main peak at 284.6 eV. Then, oxygen atoms/carbon atoms (O/C) and nitrogen atoms/carbon atoms (N/C) are calculated.

## (8) Adhesive Force of Printing Ink

A printing ink for cellophane, "CC-ST" white, (a product of Toyo Ink Mfg. Co., Ltd.) is applied to the surface of a base layer (A) of film, using a metering bar No. 6. After drying, a peeling test is conducted using a cellophane adhesive tape (registered trademark: "Cellotape", a product of Nichiban Co., Ltd.). Then, a remaining ink area on the film is determined by image processing, and evaluation is made on the basis of the following criterion:

Remaining Ink Area	Adhesion Index
95% or more	5
90% or more, but less than 95%	4
75% or more, but less than 90%	3
50% or more, but less than 75%	2
less than 50%	1

The higher the adhesion index, the better the bonding force.

Examples

The following examples are given to further illustrate the present invention.

Example 1

An isotactic homopolypropylene (isotacticity: 97%,  $[\eta]$  : 2.5) containing 0.1 wt% of stearic acid amide and 0.1 wt% of silica was fed as a raw material of a base layer (A) to one extruder and melted at 255 °C, while an ethylene-propylene-butene copolymer (hereinafter referred to simply as "BPC", ethylene component: 3.5 wt%, butene component: 5 wt%, m.p. 138 °C) containing 0.3 wt% of oleic acid amide and 0.3 wt% of silica was fed as a raw material of a cushion layer (B) to another extruder and melted at 275 °C. Both were co-extruded into sheet in a heat-melted state at 255 °C. The sheet was wound round a cooling drum for cooling, then heated to 135 °C and stretched 4.6 times in the longitudinal direction to obtain a uniaxially stretched two-layer film. Subsequently, an ethylene-methyl methacrylate-maleic anhydride terpolymer (abbreviated to "EMMA", m.p. 100 °C) as a raw material of a heat-sealing layer (C) was melt-extruded and laminated onto the surface of the cushion layer (B) of the two-layer film thus obtained. The resulting three-layer film was conducted to a tenter which had been heated to 165 °C, in which it is stretched 9 times in the transverse direction and heat-relaxed 7.8% in the width direction at 160 °C. Then, the surface of the base layer (A) was subjected to a corona discharge treatment in a mixed atmosphere of nitrogen and carbon dioxide to adjust the surface tension to 43 dyne/cm as measured by the surface tension measuring method of JIS-K-6768. Lastly, the film was taken up onto a winder. In this way there was obtained a laminated three-layer film consisting of the base layer (A) 18  $\mu$ m thick, cushion layer (B) 3  $\mu$ m thick and heat-sealing layer (C) 4  $\mu$ m thick. The results of evaluation of the film are as shown in Table 1.

Example 2

The procedure of Example 1 was repeated except that the EMMA used as the starting material of the heat-sealing layer (C) was substituted by the BPC used for forming the cushion layer (B), that is, BPC was used for both layers (B) and (C). The results of evaluation of the resulting three-layer film are as shown in Table 1.

Example 3

A uniaxially stretched film of (A)/(B) was obtained in the same way as in Example 1 and it was then fed to a tenter, followed by the same procedure as in Example 1, to afford a laminated two-layer film of (A)/(B).  
 5 The thickness of the base layer (A) was 18  $\mu\text{m}$  and that of the cushion layer (B) was 3  $\mu\text{m}$ . Then, using another extruder in an off-line, polypropylene (LS-712, a product of Showa Denko K.K.) was heat-melted at 280 °C and in this melted state it was extruded and laminated as a heat-sealing layer (C) having a thickness of 20  $\mu\text{m}$  onto the surface of the cushion layer (B).

10 Comparative Example 1

The procedure of Example 1 was repeated except that the longitudinal and transverse stretch ratios were changed to 7.5X and 15.5X, respectively. The degree of surface orientation  $P_A$  of the base layer (A) thus formed was larger than the upper limit defined in the present invention.

15

Comparative Example 2

The procedure of Example 1 was repeated except that the heating temperature in the longitudinal stretching and the transverse stretch ratio were changed to 95 °C and 14X, respectively. The degree of surface orientation  $P_B$  of the cushion layer (B) thus formed was larger than the upper limit defined in the present invention.

20

Comparative Example 3

25 The procedure of Example 1 was repeated except that the heating temperature in the transverse stretching was changed to 200 °C. The degree of surface orientation  $P_C$  of the heat-sealing layer (C) thus formed was smaller than the lower limit defined in the present invention.

Comparative Example 4

30

The procedure of Example 2 was repeated except that the heating temperature and stretch ratio in the longitudinal stretching were changed to 160 °C and 2.5X, respectively, and those in the transverse stretching were changed to 200 °C and 4.5X, respectively. The degree of surface orientation  $P_A$  of the base layer (A) thus formed was smaller than the lower limit specified in the invention.

35

Comparative Example 5

The procedure of Example 1 was repeated except that the cushion layer (B) was not provided.

40 Comparative Example 6

In Example 1, EMMA was used as the raw material of the cushion layer (B) to obtain a three-layer film wherein the degree of surface orientation of the cushion layer (B) and that of the heat-sealing layer (C) were the same ( $P_B = P_C$ ). Other conditions were the same as in Example 1.

45

Comparative Example 7

The procedure of Example 1 was repeated except that the material melting temperature for the heat-sealing layer (C), the heating temperature in the tenter and the transverse stretch ratio were changed to 190 °C, 145 °C and 10X, respectively. As a result, the degree of surface orientation  $P_C$  of the heat-sealing layer (C) was too large, exceeding the upper limit specified in the invention.

50

The results of evaluation made in the above working and comparative examples are all shown in Table 1. From the same table it is seen that the laminated three-layer films prepared in Examples 1, 2 and 3 according to the present invention wherein the three layers are restricted in the degree of surface orientation are superior in sealability under reduced pressure, difficult to burst when sealed as bag, exhibit a strong heat-sealing force and are also superior in rigidity, hot tack and printability.

55

On the other hand, in Comparative Example 1, printability is poor because the degree of surface orientation  $P_A$  of the base layer (A) is too large. In Comparative Example 2, the film obtained is inferior in

point of bag-burst preventing property under reduced pressure and sealability because of too large surface orientation degree  $P_B$  of the cushion layer (B). In Comparative Example 3, the film obtained is inferior in point of hot tack because of too small orientation degree  $P_C$  of the heat-sealing layer (C). In Comparative Example 4, the film obtained is inferior in rigidity because of too small surface orientation degree  $P_A$  of the base layer (A). In Comparative Example 5, the film obtained is inferior in point of bag-burst preventing property under reduced pressure and sealability.

In Comparative Example 6, the film obtained is inferior in point of bag-burst preventing property under reduced pressure and sealability because although the cushion layer (B) is present the degree of surface orientation thereof is the same as that of the heat-sealing layer (C) and hence does not satisfy the condition of  $P_B < P_C$ .

Further, in Comparative Example 7, the heat-sealing force is weak because the degree of surface orientation  $P_C$  of the heat-sealing layer (C) is too large.



Table 1

No.	Polymer and Degree of Surface Orientation, P							B.B.P. Property	Sealability	Rigidity (kg/mm <sup>2</sup> )	Hot Tack (mm)	Surface Atomic Ratio of Layer (A)		Adhesive Force of Printing Ink
	Base Layer (A)		Cushion Layer (B)		Heat-Sealing Layer (C)		Heat-Sealing Force (g/cm)							
Polymer	P <sub>A</sub>	Polymer	P <sub>B</sub>	Polymer	P <sub>C</sub>					O/C	N/C			
Ex.1	PP	12.5	BPC	2.5	EMA	3.0	890	⊙	⊙	3.4	2.1	0.13	0.01	5
Ex.2	PP	12.3	BPC	2.0	BPC	3.0	660	⊙	⊙	3.3	2.0	0.14	0.02	5
Ex.3	PP	12.7	BPC	2.6	PP	2.5	815	⊙	⊙	3.1	1.6	0.13	0.01	5
Com.Ex.1	PP	16.5	BPC	2.5	EMA	3.0	880	⊙	⊙	3.7	2.2	0.08	0.004	2
Com.Ex.2	PP	12.5	BPC	3.8	EMA	3.0	715	×	×	3.5	2.2	0.10	0.01	5
Com.Ex.3	PP	12.5	BPC	2.5	EMA	1.8	770	⊙	⊙	3.6	26.0	0.11	0.01	5
Com.Ex.4	PP	1.9	BPC	2.0	BPC	3.0	600	⊙	⊙	2.1	5.0	0.12	0.02	5
Com.Ex.5	PP	12.5	non		EMA		3.0	705	×	×	4.5	0.11	0.01	5
Com.Ex.6	PP	12.5	EMA	3.0	EMA		3.0	730	△	△	5.0	0.11	0.01	5
Com.Ex.7	PP	12.5	BPC	2.5	EMA		4.5	260	⊙	⊙	2.5	0.11	0.02	5

## Effect of the Invention

The laminated three-layer film of the present invention is superior in all of bag-burst preventing property under reduced pressure, sealability, heat-sealability, hot tack, rigidity and printability because the degree of

surface orientation of each constituent layer is within a specific range defined in the invention.

## Claims

- 5 1. A laminated three-layer film comprising a base layer (A) formed by a biaxially oriented film of a crystalline polypropylene, a cushion layer (B) formed by a film of an olefin polymer having a melting point lower than that of the base layer (A), and a heat-sealing layer (C) formed by a film of an olefin polymer, wherein said layers (A), (B) and (C) are laminated in the order of (A)/(B)/(C) and have surface orientation degrees falling under the following ranges, and when the cushion layer (B) and the heat-sealing layer (C) are of the same composition, the degree of surface orientation of the cushion layer (B) is smaller than that of
 

10 the heat-sealing layer (C):  $2.0 \leq P_A \leq 15.0$   
 $0 \leq P_B \leq 3.5$   
 $2.0 \leq P_C \leq 4.0$

15 where,

$P_A$ : degree of surface orientation of the base layer (A)  
 $P_B$ : degree of surface orientation of the cushion layer (B)  
 $P_C$ : degree of surface orientation of the heat-sealing layer (C)

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2. A laminated three-layer film as set forth in claim 1, wherein said crystalline polypropylene has a melting point of not lower than 155 °C and an intrinsic viscosity  $[\eta]$  of 1.5 to 2.5 dl/g.
- 25 3. A laminated three-layer film as set forth in claim 1, wherein said cushion layer (B) is formed by an olefin copolymer having a melting point of 80 ° to 155 °C.
4. A laminated three-layer film as set forth in claim 1, wherein said cushion layer (B) has a thickness of 1 to 5  $\mu\text{m}$ .
- 30 5. A laminated three-layer film as set forth in claim 1, wherein said heat-sealing layer (C) is formed by an olefin copolymer.
6. A laminated three-layer film as set forth in claim 1, wherein the olefin polymer which constitutes the cushion layer (B) and the olefin polymer which constitutes the heat-sealing layer (C) are of the same composition, and the degree of surface orientation of the cushion layer (B) is smaller by at least 0.5 than that of the heat-sealing layer (C).
- 35 7. A laminated three-layer film as set forth in claim 1, wherein as atomic ratios within 10 nm from the surface of said base layer (A), O/C and N/C ratios are in the ranges of 0.1 to 0.35 and 0.005 to 0.05, respectively.
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# INTERNATIONAL SEARCH REPORT

International Application No PCT/JP91/01107

<b>I. CLASSIFICATION OF SUBJECT MATTER</b> (If several classification symbols apply, indicate all) <sup>6</sup>		
According to International Patent Classification (IPC) or to both National Classification and IPC		
Int. Cl <sup>5</sup> B32B27/32, B32B27/28		
<b>II. FIELDS SEARCHED</b>		
Minimum Documentation Searched <sup>7</sup>		
Classification System	Classification Symbols	
IPC	B32B27/00-27/32, 7/02	
Documentation Searched other than Minimum Documentation to the extent that such Documents are included in the Fields Searched <sup>8</sup>		
Jitsuyo Shinan Koho 1926 - 1991 Kokai Jitsuyo Shinan Koho 1971 - 1991		
<b>III. DOCUMENTS CONSIDERED TO BE RELEVANT <sup>9</sup></b>		
Category <sup>10</sup>	Citation of Document, <sup>11</sup> with indication, where appropriate, of the relevant passages <sup>12</sup>	Relevant to Claim No. <sup>13</sup>
A	JP, A, 3-76647 (Nippon Unicar K.K.), April 2, 1991 (02. 04. 91), Claim, (Family: none)	1-7
A	JP, U, 59-21943 (Dainippon Printing Co., Ltd.), February 10, 1984 (10. 02. 84), Claim	1-7
A	JP, B1, 48-44667 (Toray Industries, Inc.), December 26, 1973 (26. 12. 73), Claim, (Family: none)	1-7
A	JP, A, 50-2082 (Nippon Unicar K.K.), January 10, 1975 (10. 01. 75), Claim, (Family: none)	1-7
A	JP, A, 55-50034 (Toray Industries, Inc.), April 11, 1980 (11. 04. 80), Claim & EP, A, 10,632 & US, A, 4,297,187	7
<sup>10</sup> Special categories of cited documents: "A" document defining the general state of the art which is not considered to be of particular relevance "E" earlier document but published on or after the international filing date "L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified) "O" document referring to an oral disclosure, use, exhibition or other means "P" document published prior to the international filing date but later than the priority date claimed "T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention "X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step "Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art "Z" document member of the same patent family		
<b>IV. CERTIFICATION</b>		
Date of the Actual Completion of the International Search		Date of Mailing of this International Search Report
October 23, 1991 (23. 10. 91)		November 11, 1991 (11. 11. 91)
International Searching Authority		Signature of Authorized Officer
Japanese Patent Office		

